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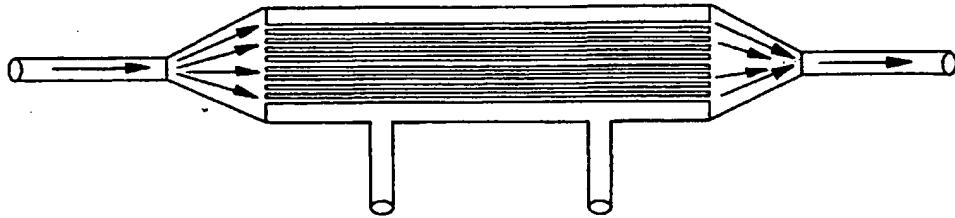
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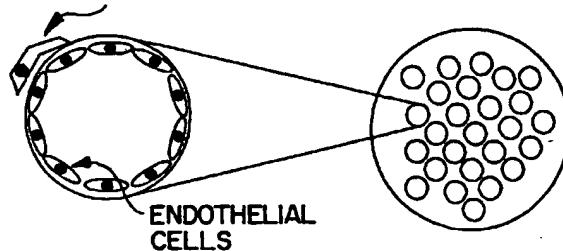
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(54) Title: CHRONIC ENDOTHELIAL CELL CULTURE UNDER FLOW



PERIVASCULAR CELL



(57) Abstract

Cells such as endothelial cells or cells transfected with a gene are attached as a monolayer on the surface of a device by growing the cells in contact with the surface under a shear stress of about 0.4 dyne/cm<sup>2</sup> to about 33 dyne/cm<sup>2</sup>. The surface may be coated with a protein such as fibronectin, laminin or collagen. In a specific embodiment, the device is a cartridge containing polypropylene hollow fibers and the cells are grown in the inner lumen of the hollow fibers which have been coated with the protein. Shear stress is controlled by the rate of medium flow through the lumen. In another embodiment, the monolayer of cells is formed on an implantable prosthetic device such as a vascular graft for use in vivo. Cells are grown in the inner lumen of a vascular graft and/or in a chamber surrounding the vascular graft while controlling medium flow through the lumen and/or surrounding chamber to provide the shear stress.

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## CHRONIC ENDOTHELIAL CELL CULTURE UNDER FLOW

### BACKGROUND OF THE INVENTION

This patent application is a continuation-in-part of application Serial Number 08/054,794, filed on April 28, 1993.

#### 5      1. Field of the Invention

The present invention relates generally to culture of cells *in vitro* and specifically to an *in vitro* method of producing a device coated with adherent endothelial cells under conditions of prolonged, continuous shear stress.

#### 2. Description of the Related Art

- 10      Culture of endothelial cells *in vitro* is most commonly performed under static conditions such as in a culture dish or flask with stationary medium. However, since endothelial cells form the inner lining of blood vessels, they are normally exposed to continuously flowing blood as opposed to static conditions. This creates varying degrees of chronic shear stress that acts on the endothelial cells.
- 15      Even during blood vessel development (angiogenesis), endothelial cells are continuously exposed to flow, and are never in a static environment. It is therefore desirable to study the biology of endothelial cells and prepare the cells for use *in vivo* under conditions closely resembling those *in vivo*, specifically under chronic shear stress.
- 20      Shear stress is the frictional force produced by fluid as it moves past a solid.

Shear stress is dependent on the configuration of the fluid path, the viscosity of the fluid and the rate of fluid flow. For cylindrical tubes containing flowing Newtonian fluid, shear stress is calculated as follows:

$$5 \quad = \frac{4 n Q}{\pi r^3}$$

where n=dynamic viscosity, Q=flow rate and r=inner radius of the cylinder.

- In vitro* systems previously described for the study of shear stress on endothelial cells fall into three groups, namely cone-plate rheometers, parallel plate perfusion systems and glass capillary perfusion systems. The cone-plate rheometer consists of a flat plate over which is suspended a rotating cone (Dewey, et al., *J.Biomech.Engr.*, 103:177, 1981; Davies, et al., *Proc.Natl.Acad.Sci. USA*, 83:2114, 1986; Ando, et al., *Biorheology*, 27:675, 1990). The angle between plate and cone, the rate of rotation of the cone and the viscosity of the fluid between plate and cone determine the shear stress to which cells growing on the plate are exposed. Advantages of this system are that the shear stress can be accurately determined, that shear stress can be varied instantaneously and can be varied without concomittant changes in hydraulic pressure, and, with modification, the system allows direct observation of the cells under shear stress.
- 20 The parallel plate perfusion system consists of two glass plates brought in close apposition, with one of the plates containing the cells (Wechezak, et al., *J.Cellular Physiol.* 139:136, 1989; Gupte et al, *In Vitro Cell. Dev. Biol.* 26:57, 1990; Ando, et al., *In Vitro Cell. Dev. Biol.* 24:871, 1988; Frangos, et al., *Biotechnol. Bioengineering* 32:1053, 1988). Fluid flows between the two plates over the surface of the endothelial cells. To enhance cell adhesion, the glass is pretreated with NaOH, which confers a negative charge to the glass. The advantages of the system are that it allows ready access to the cells for
- 25

microscopic observation, and that it is technically much simpler and therefore less expensive than the cone-plate apparatus.

The glass capillary perfusion system consists of glass capillary tubes into which the endothelial cells are seeded, and through which medium flows (Olesen, et al., *Nature*, 331:168, 1988; Hohn, et al., *Int.J.Microcirc:Clin.Exp.*, 9:411, 1990). Given the cylindrical nature of the capillary, shear stress tends to be rather uniform in the capillary, except at entry and exit points, an assumption that cannot be as easily made for the parallel plate apparatus. The principal advantage of this system lies in its simplicity, and presumably, the low cost. In addition, cells located at the exit point of the capillary are accessible for patchclamp work.

One problem found in prior art systems described include growth of only a limited number of cells (e.g.  $10^5$  cells) at any given time under any given condition. Therefore, studies in which significant quantities of RNA or cell culture supernatants must be harvested cannot be done. Large quantities of RNA are required to establish cDNA libraries, to perform Northern blotting analyses and to perform RNase protection assays. Also, large quantities of cell supernatants are required to characterize and purify materials secreted by the cells under flow.

Most of the current systems allow study under shear stress for only a brief period of time (minutes to hours). Typically, existing systems require that cells be established first under static conditions, and then switched to flow conditions. The effect of flow, with its accompanying shear stress, is then interpreted by comparing cells under static conditions to those under flow conditions. However, the switch from static to flow conditions is a very unphysiologic stimulus. Cells grown under static conditions are poorly differentiated and poorly adherent. Application of flow (and therefore shear

stress) suddenly causes a significant number of cells to dislodge. Also, it is not obvious that acute effects of shear stress application on static cells resemble physiologic effects *in vivo* during alterations in the level of shear stress. Therefore, it would be desirable to have a system in which cells could be adapted to chronic shear stress from the time of seeding, producing adherent and differentiated endothelial cells, which would more closely reflect the *in vivo* situation.

The study of chronic cell-cell interactions *in vitro* necessitates co-culture of distinct cell types in such a way that the cells are kept separate but are able to interact. The importance of co-culture lies in the fact that a large number of cell-cell interactions occur in the perivascular space *in vivo* and these interactions are likely to be influenced by endothelial cells exposed to chronic shear stress. The present systems cannot accomplish co-culture in this manner, first because other systems utilize impermeable cell culture supports, second because application of acute shear stress causes the endothelial cells to dislodge, and third because endothelial cells not adapted to chronic shear stress remain poorly differentiated.

All of the existing systems described above utilize culture material such as glass or plastic which are not similar to that used for vascular grafts in humans. Thus, existing systems for the study of endothelial cell shear stress do not mimic the behavior of endothelial cells on clinically useful prosthetic vascular materials. A desirable system would allow the study of the effects of shear stress on endothelial cell adhesion to prosthetic surfaces pertinent to clinical use.

Artificial vascular grafts suffer the shortcoming that the materials tend to be thrombogenic, thus limiting their use to larger vessels. Production of grafts of small caliber made non-thrombogenic by an established monolayer would be a great advance in vascular surgery. However, endothelial cell adhesion is  
5 usually poor when the cells are pre-seeded onto artificial material under static conditions.

The ease with which endothelial cells of animal origin will replicate on artificial prostheses *in vitro* mimics the *in vivo* environment in which growth of endothelial cells onto vascular grafts from anastomotic sites is only a few centimeters. It would be desirable to exploit the ability of endothelial cells to  
10 replicate in static culture and form confluent monolayers when seeded *in vitro* on implantable biomaterials to develop prostheses containing endothelial monolayers which can maintain their integrity under *in vivo* conditions. Such prostheses would allow the utilization of techniques useful for the treatment of  
15 a variety of diseases.

The present invention addresses the needs of the scientific and medical community by providing a method for producing a device coated with highly adherent cells wherein the cells more accurately reflect the growth pattern observed *in vivo*.

SUMMARY OF THE INVENTION

The present invention arose from the discovery of a method for producing a device coated with a firmly adherent cell monolayer. The inventors have determined that the culture of endothelial cells under prolonged, continuous shear stress accurately mimics the differentiated *in vivo* endothelial cell environment and phenotype, in contrast to previous methods utilizing static culture conditions and proliferating cells. A device produced by the method of the invention is useful for vascular grafts, including artificial heart valves, vascular stents, vascular access grafts for dialysis or other forms of hemoperfusion and any implantable device containing artificial blood vessels or capillaries, in which non-endothelial cells are co-cultured with endothelial cells.

**BRIEF DESCRIPTION OF THE DRAWINGS**

FIGURE 1 shows schematically the configuration of the cell culture cartridge. Also shown is the location of growing cells in a cross-section of a fiber.

FIGURE 2 shows endothelial cells grown under 0 shear stress.

5 FIGURE 3 shows cells grown at high flow acute (HFA) (13-15 dyne/cm<sup>2</sup> for the last day of nine days of culture).

FIGURE 4 shows scanning and transmission electron microscopy (EM) studies of cells grown under flow.

FIGURE 5a shows the expression of actin in cells grown under flow.

10 FIGURE 5b shows scanning and transmission EM scanning and transmission EM of cells grown under static conditions.

FIGURE 5c shows scanning and transmission EM of cells grown under shear stress flattened with fenestral formation.

15 FIGURE 5d shows scanning and transmission EM of Weibel Palade bodies of cells grown under shear stress.

FIGURE 5e shows scanning and transmission EM of a polypropylene fiber containing glomerular endothelial cells adapted to shear for 9 days.

FIGURE 6 shows the mitogenic effect of endothelial cell conditioned medium on quiescent glomerular epithelial cells.

FIGURE 7 shows a Northern blot analysis of total RNA from endothelial cells under flow and probed with PDGF-A and PDGF-B chain cDNAs.

FIGURE 8 shows a radioassay of PGF<sub>1 $\alpha$</sub>  accumulation in cells grown under static, LFC, HFA and HFC conditions.

5 FIGURE 9 shows a diagram of the vascular graft flow chamber.

FIGURE 10 shows the number of cells dislodged by an acute pulse of shear stress (25 dynes/cm<sup>2</sup> for 25 sec) from endothelial cell seeded grafts after 6 days of culture in the absence of presence of chronic shear stress. (Mean  $\pm$  SE, p <0.05).

10 FIGURE 11 shows light and electron microscopy of grafts after exposure to an acute pulse of shear stress (25 dynes/cm<sup>2</sup> for 25 sec). Panels A, C, E: grafts cultured with continuous shear stress for 6 days. Panels B, D, F: grafts cultured in the absence of luminal shear stress for 6 days. A, B: 60X; c, D: 160X (longitudinal sections, H & E stain). Intact monolayers of endothelial cells are shown on the luminal surface (L) of grafts cultured in the presence of shear stress (>). Few cells are present on the luminal surface of grafts cultured without luminal shear stress (-). Cells are present on the abluminal surface ( $\dagger$ ) and in the interstices of the grafts. E, F: Scanning electron microscopy of graft lumens, 100X.

20 FIGURE 12 shows whole blood clotting time in vascular grafts. Endothelial cell free grafts (n=4), grafts seeded with endothelial cells and cultured without luminal shear stress (n=6) or with luminal shear stress (n=6). Lines connect individual data points obtained from grafts within a single experiment and with the same blood sample. The clotting time was 41  $\pm$  4 percent longer in grafts

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cultured with luminal shear stress compared to grafts cultured without luminal shear stress ( $p<0.01$ ).

DETAILED DESCRIPTION OF THE INVENTION

The present invention provides a method for producing a device having a surface coated with a firmly adherent cell monolayer. The method comprises culturing the adherent cells in the presence of the surface of the device under 5 conditions of continuous shear stress to produce the monolayer on the surface. The device produced by such a method is useful as an implantable structure *in vivo*.

Certain basic problems in growing cells to densities and/or to structures approaching those of living tissues include problems with a means of supplying 10 nutrient medium to the cells. The present invention provides a method of culturing cells which overcomes many of the basic problems associated with producing an artificial organ-like device *in vitro* which can be utilized *in vivo*.

Producing an artificial organ-like device *in vitro* which contains an adherent cell monolayer or a surface of the device faces various problems. One problem 15 is that components of the medium must diffuse through the cell layers to reach all cells; this diffusion becomes more difficult as the thickness of the cell layer increases. Circulation of medium through hollow fibers, also termed artificial capillaries, on whose outer surface organ-like cells are grown, circumvents this problem *in vitro* (US Patent No. 3,883,393). However, if blood is circulated 20 through the hollow fibers, as would occur if the hollow fibers, with organ-like cells on their outer surface, were implanted into the blood stream *in vivo*, coagulation of blood in the hollow fibers would occur unless the fibers were lined on their inner surface, by a confluent, adherent and differentiated monolayer of endothelial cells.

Another problem associated with growing an artificial organ-like device *in vitro* is the maintenance of a suitable microenvironment in conventional cell culture. A constant supply of medium can be assured *in vitro* by circulating the medium through permeable hollow fibers permeating the artificial organ. A supply of mediators normally produced *in vivo* by endothelial cells is not possible unless the permeable hollow fibers contain, on their inner surface, a confluent layer of endothelial cells analogous to those living surfaces of living tissues. However, until the present invention production and maintenance of such a layer of endothelial cells which resists the *in vivo* shear stress of flowing medium, such as blood, for prolonged periods of time has not been achieved in devices where endothelial cells are first used *in vitro* to coat the device.

A third problem is the requirement of a suitable material for a lattice or suitable material upon which to grow the monolayer. In an embodiment of the present invention, cells suspended in a nutrient medium are initially allowed to settle on the surface of the device, such as capillaries or fibers, through which oxygenated nutrient medium continuously flows. Nutrient substances pass from the perfusing medium through the capillary wall and into the cell, while cell products, e.g., lactic acid and hormones, pass from the cell through the capillary wall and into the perfusate. These products may be recovered by suitable means.

The method of the present invention overcomes these problems and in one embodiment provides for growth of cells under conditions of continuous shear stress, wherein the device contains at least one cell culture unit, along with a medium reservoir, a gas exchanger, and a pump to provide controlled flow rates of the perfusate. By producing the adherent cell monolayer under continuous shear stress, the monolayer closely resembles naturally occurring firmly adherent cell layers found *in vivo*, such as the lining of blood vessels.

The device to be coated with an adherent cell monolayer can be any structure which is useful for implanting in a subject or for studies of interaction between cells and soluble factors produced by those cells. For example, the device may be an implantable biomaterial which is used as a prosthetic vascular device. Artificial vascular grafts tend to be thrombogenic thereby limiting their use to larger vessels. Production of non-thrombogenic grafts of small dimensions can be accomplished by the method of the invention. Examples of such vascular grafts include coronary artery bypass grafts, peripheral vascular bypass grafts, prosthetic heart valves and vascular access grafts for any type of hemoperfusion such as dialysis or plasmapheresis. Alternatively, the method of the invention can be used to produce an adherent cell monolayer as a surface of artificial capillaries as in a hollow fiber culture device or cartridge.

The cells used in the method of the invention are seeded directly onto a surface of the device under flow, or "continuous shear stress" *in vitro*. "Continuous shear stress" refers to the force of the medium on the cells that occurs due to continual circulation of the medium. The amount of shear stress will vary with the size, shape and contour of the device used for culture. The appropriate shear stress is dependent on the configuration of the fluid path, the viscosity of the fluid and the rate of fluid flow. These parameters can be easily determined by one of skill in the art without resorting to undue experimentation. By growing the cells under continual stress, the device more closely approximates the *in vivo* environment, for example, where blood passes over the endothelium in a blood vessel.

Cells grown according to the method of the invention should possess the property of being able to form a monolayer on a surface substrate of the device. Initial attachment of cells may be accomplished by any means which allows the cell to grow as a monolayer on a device. Attachment enhancing

surfaces can be produced directly, such as by selecting appropriate plastic polymers for the device or, indirectly, as by treating the surface in the device by a secondary chemical treatment. Therefore, "attachment" refers to the ability of a cell to adhere to a surface in a culture device, wherein the attachment promoting surface is in direct contact with the cells, which otherwise would grow in a three-dimensional cellular aggregate in suspension. Attachment, or adherence, of a cells to the device surface allows them to produce a monolayer. In the absence of shear stress, endothelial cell adhesion remains weak. Techniques for modifying surfaces for enhancing adherence of cells are well known in the art.

Preferably the cells grown by the method of the invention are grown under levels of shear from about 0.4 dyne/cm<sup>2</sup> to about 33 dyne/cm<sup>2</sup> and most preferably from about 1dyne/cm<sup>2</sup>to about 14 dyne/cm<sup>2</sup>. At these levels, the cells do not dislodge and remain sufficiently attached to the surface of the device to form an adherent monolayer.

In a preferred embodiment, the endothelial cells used in the method are seeded at confluent density ( $10^5$  cells/cm<sup>2</sup> or greater) directly onto a surface of the device. Initial adhesion takes place under static conditions during 45-60 minutes. Shear stress is then applied in a graded fashion, at no more than 1 dyne/cm<sup>2</sup> during the first 24-96 hours, then at levels as high as 33 dynes/cm<sup>2</sup> for an additional 3 days or more. From the time of initial attachment, the application of shear stress is uninterrupted except for brief periods of time during which the culture medium is renewed. The graded shear stress conditioning of the endothelial cells causes them to differentiate and to become highly adherent to the surface of the device. Because the device with a high density of endothelial cells is preferred, a confluent monolayer is established without the necessity of cell proliferation while under shear stress. Shear stress is partly dependent on the size, shape and contour of the device used for

culture and on the rate of flow and viscosity of the medium. The appropriate level of shear stress (1-35 dynes/cm<sup>2</sup>) will vary based on such factors as whether the device is exposed to venous or arterial blood flow as well as other commonly known *in vivo* parameters. However, the influence of such factors  
5 on the selection of the appropriate shear stress parameters can be easily determined by one of skill in the art, without resorting to undue experimentation. By subjecting the endothelial cells to essentially uninterrupted shear stress for 6 or more days the device more closely approximates the *in vivo* environment, for example, where blood passes over the endothelium in a blood  
10 vessel.

In addition to interactions with soluble factors, most cells *in vivo* are in contact with an extracellular matrix, which is a complex arrangement of interactive protein and polysaccharide molecules which are secreted locally and assemble into an intricate network in the spaces between cells. According to the method  
15 of the invention, the addition of an extracellular matrix protein to the surface of the culture device forms an insoluble matrix which allows cells in culture to adhere in a manner which closely corresponds to the *in vivo* extracellular matrix. The adherent cell-coated device of the invention can be preferably produced by coating the surface of a device, such as a hollow cartridge, with  
20 a polybasic amino acid composition to allow initial attachment of the cell. Such compositions are well known in the art and include polyornithine and polylysine. Alternatively, the surface of the device may be coated with a known extracellular matrix or matrix-like protein composition to enhance the cell's ability to grow and form a monolayer on the substrate. Such compositions  
25 include laminin, collagen, fibronectin and Pronectin F. Other extracellular matrix proteins that can be used will be apparent to one of skill in the art.

In a preferred embodiment of the invention, the material on which the cells are grown is similar to that used for vascular or other grafts. Preferably, the method of the invention uses a device which is composed of polypropylene material. Alternatively, prosthetic devices composed of materials such as 5 dacron or expanded polytetrafluoroethylene can be used. Other materials which allow endothelial cell adhesion to the surface when the cells are grown under shear stress *in vitro* from the moment of seeding will be known to those of skill in the art.

Preferred adherent cells grown according to the method of the invention are 10 endothelial cells. Examples of endothelial cells include vascular, retinal capillary, glomerular, corneal, aortic and brain capillary cells. The cells may be derived from many species including bovine, rat, human, rabbit and porcine. Preferably, the cells utilized in the implant are species specific, therefore, 15 endothelial cells from a human would be used for an implant intended for a human subject, for example.

At the time of seeding, the cultures can be analyzed for endothelial cell-specific function to ensure the homogeneity of the cell population. Functional assays which are specific for endothelial cells include uptake of acetylated low density lipoprotein (LDL) and the presence of von Willebrand's factor. Additionally, 20 assays for the presence of antigens specific for smooth muscle cells, such as alpha and gamma-actin isoforms, can be used to rule out potential contamination with smooth muscle cells.

The method of the invention allows cells to be co-cultured in combination with other cell types in the device. "Co-culture" refers to the growth of more than 25 one type of cell in a shared environment so that the cells are physically separated, but still able to interact such that growth factors and other secreted soluble mediators produced by a cell can interact with another cell.

This type of co-culture is similar to the *in vivo* environment where cell-cell interactions occur in the perivascular space, for example. Typically, these interactions are influenced by endothelial cell shear stress and, as a result, the method of the invention closely resembles the *in vivo* situation.

5       The method of the invention for culturing cells typically entails co-culture of two types of cells, preferably endothelial cells and perivascular cells. Preferred perivascular cells are vascular smooth muscle cells, mesangial cells, pericytes, fibroblasts or epithelial cells for example.

10      The cells may be grown using a hollow cartridge device which contains at least one fiber for growth of the cells. The lumen inside the fibers is referred to as the inner lumen and the lumen outside the fibers is referred to as the outer lumen. Preferably, endothelial cells are grown in the inner lumen and perivascular cells are grown on the outer lumen. Media flows continuously through the inner lumen thus creating a constant shear force which is physiologically similar to the *in vivo* environment of vascular tissue.

15      The cells grown by the method of the invention can be transfected with a gene. A major complication of current interventions for vascular disease, such as balloon angioplasty or endarterectomy, is disruption of the artherosclerotic plaque and thrombus formation at sites of local tissue trauma. Genetically altered endothelial cells could minimize local thrombosis. In addition, such altered cells grown using the method of the invention may be useful for the treatment of myocardial or tissue ischemia by introducing cells expressing thrombolytic, angiogenic, or growth factor genes into the graft. Because of its contiguity with the bloodstream, the endothelium is an attractive target for the delivery of functional genes *in vivo*. The use of endothelium for gene transfer would permit secretion of a recombinant protein from genetically engineered endothelial cells directly into the blood. Alternatively, endothelial cells

expressing a nonsecreted recombinant protein might be able to inactivate a toxic substance that is circulating in the blood.

For transfection of a eukaryotic cell, such as an endothelial cell, standard methods of transfection of DNA including calcium phosphate co-precipitates, 5 conventional mechanical procedures such as microinjection, insertion of a plasmid encased in liposomes, or virus vectors may be used. Eukaryotic cells can also be cotransformed with DNA sequences encoding a gene product of interest, and a second foreign DNA molecule encoding a selectable phenotype, such as the herpes simplex thymidine kinase gene (*Current Protocols in Molecular Biology*, Wiley Interscience). Another method is to use a eukaryotic viral vector, such as simian virus 40 (SV40) or bovine papilloma virus, to transiently infect or transform eukaryotic cells and express the protein. 10 (*Eukaryotic Viral Vectors*, Cold Spring Harbor Laboratory, Gluzman ed., 1982).

Isolation and purification of expressed polypeptides, or fragments thereof, produced *in vitro* by the cells grown according to the method of the invention, 15 may be carried out by conventional means including preparative chromatography and immunological separations involving monoclonal or polyclonal antibodies. Such techniques are standard and common in the art.

Genes which may be transfected into cells forming the monolayer include 20 genes which encode proteins which promote angiogenesis, reduce thrombosis, promote repopulation, inhibit neo intimal smooth muscle cell hyperplasia, mediate vasodilation or other therapeutic proteins. For example, endothelial cells could be transfected with t-PA (Friezner, et al., *J. Biol. Chem.* 261:6972, 1986) or PLA<sub>2</sub> (Sharp, et al., *J. Biol. Chem.*, 266:14850, 1991) to inhibit 25 thrombogenicity. Other examples include the incorporation of the vascular endothelial growth factor gene to selectively promote angiogenesis in the absence of smooth muscle proliferation (Fischer, et al., *J. Biol. Chem.*,

266:11947, 1991) or transfecting cells with the NO synthase gene (Marsden, et al., FEBS, 307:287, 1992) in order to overproduce the vasodilator nitric oxide.

The following examples are intended to illustrate, but not limit the invention. While they are typical of those that might be used, other procedures known to  
5 those skilled in the art may alternatively be utilized.

### EXAMPLES

Prosthetic vascular grafts with adherent endothelial cell monolayers may prove useful for small caliber vessel bypass. However, endothelial cells adhere poorly to prosthetic graft material, causing them to be stripped when exposed to *in*  
10 *vivo* shear stress. These examples show that shear stress, imposed stepwise *in vitro*, improves endothelial cell adhesion and decreases the thrombogenicity of endothelial cell seeded grafts.

Less than 1% of the endothelial cells were lost from the shear stress conditioned grafts when exposed acutely to arterial shear stress. By contrast, on  
15 average 100 fold more cells were dislodged from grafts not previously exposed to shear stress. By light and electron microscopy, an intact endothelial monolayer was observed covering the lumen of shear stress conditioned grafts whereas few cells were seen on the luminal surface of grafts not previously exposed to shear stress. The clotting time in shear stress conditioned grafts  
20 was significantly prolonged in relation to grafts not exposed to shear stress. These findings demonstrate that shear stress conditioning of endothelial cell seeded grafts augments endothelial cell retention and reduces thrombogenicity of small caliber vascular grafts.

EXAMPLE 1PRODUCTION OF AN ADHERENT CELL MONOLAYER  
ON A CELL CULTURE CARTRIDGE

The 4 station pump (Cellmax Quad), gas permeable tubing and polypropylene  
5 cartridges were from Celico, Inc. (Germantown, MD). ProNectin F solution was  
from Protein Polymer Technologies, Inc. (San Diego, CA). Injection sites were  
from Quest Medical, Inc. (Dallas, TX). Cell culture media and serum were from  
Gibco BRL (Gaithersburg, MD). Glomerular endothelial cells were derived from  
bovin calf kidneys according to methods described previously (Ballermann, B.  
10 *Am.J.Physio.* 256:C182, 1989). The configuration of the cell culture cartridge  
is shown in FIGURE 1, and the location of the growing cells is shown schemati-  
cally in a cross-section of a fiber.

The male Luer lock caps were removed and the sterile cartridge was drained  
of PBS. Each port was then capped with an injection site (Quest Medical, Inc.,  
15 Dallas, TX). Once capped all of the following procedures were performed with  
syringes and 20 gauge needles. Before each injection, the injection site to be  
entered was cleaned with an alcohol swab.

With the long axis of the cartridge in the vertical position, 5 ml of a 1:20  
ProNectin F solution (Protein Polymer Technologies, Inc., San Diego, CA) was  
20 injected into the bottom port to completely fill the inner lumen of the cartridge.  
The ProNectin F solution was left in the cartridge at room temperature for 2  
hours. Every 15 minutes, the cartridge was shaken and rotated to a different  
resting plane. After 2 hours, the inner lumen was drained of the ProNectin F.

25 The cartridge was washed thoroughly with PBS as the ProNectin F diluant is  
extremely toxic to cells. The inner lumen was washed with 30 cc of sterile PBS  
followed by washing of the outer lumen also with 30 cc of sterile PBS. This

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washing procedure was repeated three times and then both lumens were drained of PBS. The inner and outer lumens were filled with media containing 1% fetal bovine serum.

Endothelial cells were trypsinized from cell culture plates and suspended in 5 ml of RPMI with 1% FBS to achieve a cell concentration of  $0.5\text{--}1.0 \times 10^7$  cells/ml, and injected into the cartridge. The cartridge was turned so that the long axis was horizontal with the side injection ports vertical and placed in the incubator at 37°C in an atmosphere of 5% CO<sub>2</sub> in air for 45 minutes. A second cell suspension of similar concentration was then prepared and injected into the cartridge. The cartridge long axis was again placed horizontal and the cartridge rotated 90 degrees so that the side injection ports were horizontal. The cartridge was placed into the incubator for 45 minutes. This process was repeated two more times, each time rotating the cartridge 90 degrees, so that the inner lumen of the cartridge was turned a full 360 degrees about its long axis. After the last 45 minute incubation, the cartridge was gently flushed with 15 cc of RPMI with 15% FBS and FGF (4 ng/ml) and the outer lumen was flushed with 30 cc of the same.

The reservoir tubing and ball valve apparatus were filled with medium by removing the male Luer lock caps from the sterile tubing and joining both ends with a double male Luer lock adaptor (Cobe, Lakewood, CO). The reservoir was filled with 70 mls of medium and was hand pumped through the system until the entire circuit was filled with medium. Approximately 20 cc was required to fill the tubing. The tubing was then clamped on either side to prevent any flow.

The tubing on the now seeded cartridge was also clamped on each long axis end. With the cartridge long axis horizontal, the injection site was removed from the end of the cartridge. The pump tubing containing the double male

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Luer lock adaptor was unscrewed so that the adaptor remained on the thicker tubing which comes directly from the pump and is the inflow tubing. This was then hooked onto the open cartridge inflow port. (It is important to keep the amount of air in the inflow system to a minimum).

5      A second double male Luer lock adaptor was hooked to the open pump outflow tubing. The injection port was removed from the other end of the cartridge and that was joined to the open end of the double male Luer lock adaptor (this then became the outflow port). Invariably there will be some air in the system on the outflow side, but it will be removed when the medium circulates through the reservoir. It is important to avoid air bubbles from passing through the cartridge as they will strip cells off the fibers. Air bubbles can also collect on the inflow port and produce an airlock on some of the upper fibers thereby preventing equal flow to all the fibers.

15     The clamped tubing was unclamped and the cartridge and tubing was hand pumped a few times to assure proper flow. The system was then connected to the mechanical pump. Flow was started at the lowest setting for several days to allow the cells the best opportunity to attach. The medium was changed every two days. To vary the viscosity, dextran (70-2000) was added to the culture medium at a concentration of 5-10%. The medium was then sterile filtered. The viscosity was measured with a Cannon-Manning semi-micro capillary tube viscometer (International Research Glassware, Kenilworth, NJ).

EXAMPLE 2  
GLOMERULAR CELL CULTURE

For the culture of glomerular endothelial cells under flow, hollow fiber cartridges containing bundles of 175 or 230 polypropylene fibers each 13 cm in length and 330  $\mu\text{m}$  in diameter were used. The cartridges are similar in design to hemodialysis cartridges, namely medium can be circulated independently through the inner lumen and around the external surface of the hollow fibers. A medium reservoir was connected to the hollow fiber cartridge via gas permeable tubing. The tubing contains a compressible chamber with two unidirectional valves at the entry and exit ports (pumping chamber). The pump system contains 4 pump heads which operate by cyclical compression of the pumping chamber, thus producing unidirectional flow (FIGURE 1).

The pump system and the flow paths with the hollow fiber cartridges all sit in a water-jacketed cell culture incubator in humidified atmosphere of 5% CO<sub>2</sub> in air. The pump rate is adjusted with a control unit which sits outside the incubator. In addition, the pump heads are exchangeable such that the degree of compression of the pump chamber can be controlled independently. Control of the pump speed and pump head size allow variations in the rates of fluid flow ranging from 2.5 to 50 ml/min. This translates to a calculated shear stress in each fiber of ~1 to 20 dyne/cm<sup>2</sup>, assuming a medium viscosity the same as water. For these experiments the medium viscosity is adjusted under dextrans. The range of shear stress achieved in the presence of 5% dextran-70 is ~3-60 dyne/cm<sup>2</sup>. In each experiment (and for each change in pump speed/pump head size), medium flow rates are measured independently by determining the fluid volume exiting each cartridge as a function of time. The CellMax Quad system was adapted by the PI for endothelial cell culture during the past 2 years. This system was not previously used for culture of cells in the lumen of the fibers under flow.

Fluid viscosity is determined independently using a Cannon-Manning semi-micro capillary tube viscometer (International Research Glassware, Kenilworth, NJ) which is suspended in a water bath at 37°C. For the purpose of these studies, it is assumed that the level of shear stress does not significantly alter  
5 fluid viscosity.

Glomeruli were isolated under sterile conditions from bovine calf kidneys obtained from a local slaughterhouse (Ropersberger's, Baltimore) as previously published (Ballermann, B., *Am. J. Physiol.*, **256**:C182, 1989). The purity of the preparation was checked by microscopy; glomerular preparations less than  
10 95% pure are discarded. The glomeruli were subjected to collagenase (CLS III, Worthington) digestion for 45 minutes at 37°C. Glomerular remnants were removed by centrifugation for 5 minutes at 100 x g. The remaining cell suspension was sedimented at 800 x g (5 minutes), and plated at cloning density on gelatin-coated plates in RPMI 1640 medium containing 15% fetal  
15 bovine serum, 8 ng/ml acidic FGF (R&D Systems Inc., Minneapolis) and 0.1 µg/ml heparin (Sigma) and incubated in a humidified atmosphere of 5% CO<sub>2</sub> in air. Cloning density refers to the dilution of cells at which 5-15 single colonies form per 100 cm<sup>2</sup>. To achieve this, serial dilutions of the primary cell suspension ranging from 1:10-1:10,000 are plated. Typically, cells plated at  
20 1:100 to 1:1000 are at cloning density. The medium was changed every 48 hours and when endothelial cell colonies appeared (usually 10-14 days after plating), they were selected with cloning cylinders, detached with trypsin/EDTA and passed to new plates again at cloning density. Usually new endothelial cell clones appeared within 10 days. These were again selected with cloning  
25 cylinders, detached with trypsin/EDTA and individual colonies passed to wells of 12-well plates. Once cloned, the primary endothelial cells were expanded. For expansion, the endothelial cells were passed just prior to reaching confluence at a 1:3 split. Once the cells were no longer at cloning density the concentration of α-FGF was reduced to 4 mg/ml. All of the cultures were

- performed on gelatin-coated plates. The cells were cloned twice because after the first round of cloning many of the cultures still contained a few mesangial cells, which overgrew the culture within a few weeks if not removed. The identity of the endothelial cells was always verified using acetylated LDL uptake.
- 5 To visualize acetylated LDL uptake, endothelial cells were grown on glass coverslips, washed with medium containing 2% serum, and then incubated with 10 mg/ml fluorescent acetylated LDL (Biomedical Technologies, Stoughton, MA) for 3 hours. Cells were then washed with PBS and observed by fluorescence microscopy.
- 10 The inner lumen of the polypropylene fibers was first coated with 0.05 mg/ml Pronectin F (Protein Polymer Technologies, Inc.) in PBS for 2 hours, followed by extensive washing of the inner and outer aspects of the fibers with PBS. Cells harvested with trypsin/EDTA from static culture plates were then introduced at a concentration of  $\sim 5 \times 10^6$  cells/ml in RPMI 1640 medium
- 15 containing 1% PBS to fill the lumen of the fibers ( $\sim 5$  ml). Pronectin F is a synthetic protein polymer containing multiple repeats of the RGD fibronectin binding site. During attachment the serum concentration in the medium was kept low to prevent competitive interaction of cell integrins with soluble fibronectin in serum. After 45 minutes of incubation at 37°C in a humidified atmosphere of 5% CO<sub>2</sub> in air with the cartridge in the horizontal plane, unattached cells are gently flushed out, and the seeding protocol is repeated an additional 3 times, each time the cartridge is rotated 90° to assure circumferential cells attachment. At the end of the fourth attachment period, the medium was replaced with RPMI 1640 containing 15% serum and 4 ng/ml
- 20  $\alpha$ -FGF with 0.1  $\mu$ g/ml heparin and the cartridges were connected to flow at venous (1-1.5 dyne/cm<sup>2</sup>) levels. The medium was changed every 48 hours.
- 25

Glomerular endothelial cells were seeded into Pronectin-F coated polypropylene fibers, and maintained in culture for 9 days. In some of the cartridges medium was continually circulated around the extraluminal surface of the fibers (0 shear stress). Some of the cartridges were kept at venous levels of shear  
5 for nine days ( $\sim 1.5$  dyne/cm $^2$ ) (Low Flow Chronic, LFC). In some of the cartridges, venous levels of shear were used initially, and then arterial levels of shear (13-15 dyne/cm $^2$ ) were imposed for the last 1 (High Flow Acute, HFA) or 5 (High Flow Chronic, HFC) days of the nine day period. Cells grown on  
10 Pronectin F coated plastic cover slips in cell culture plates served as additional "static" controls. Cells were then fixed and processed for transmission and scanning electron microscopy.

*Adhesion:* Cells grown in cartridges with 0 Shear stress initially attached. However, after 9 days in culture, acute shear stress at a level of  $\sim 10$  dyne/cm $^2$  to cells accustomed to a no stress environment; removed most of the cells  
15 from the cartridge. By contrast, the same level of shear stress did not dislodge the cells that had been grown under flow. Table 1 shows one experiment each for bovine glomerular (GEN) and bovine aortic (BAE) endothelial cells. The cells grown chronically under shear stress adhered more firmly to the fibers than cells not previously accustomed to shear.

**TABLE 1**  
**NUMBER OF CELLS DISLODGED AFTER ADAPTATION**  
**TO VARIOUS SHEAR STRESS CONDITIONS**

5	CHRONIC SHEAR LEVEL	GEN-1 <sup>a</sup>	GEN-2 <sup>b</sup>	BAE ( $\pm$ SE) <sup>c</sup>
10	0	$2390 \times 10^4$	$480 \times 10^4$	$1223 \pm 273 \times 10^4$
	LFC	$708 \times 10^4$	$43 \times 10^4$	$113 \pm 51 \times 10^4$
	HFC	$87 \times 10^4$	$11 \times 10^4$	$11 \pm 7 \times 10^4$
	HFA	$45 \times 10^4$	$4 \times 10^4$	$6 \pm 3 \times 10^4$

<sup>a,b</sup> Results of two separate experiments.

<sup>c</sup> Results of five separate experiments.

- 15      The precise total cell number contained in each cartridge could not be determined, since the cells in the cartridges accustomed to chronic flow could not be removed even with prolonged trypsin treatment. One possible explanation for the finding in Table 1 is that there were substantially fewer cells contained in the cartridges accustomed to flow. However, since scanning electron microscopy consistently showed confluent monolayers of cells in those cartridges, whereas few adherent cells were seen in the cartridge in the cartridges prepared under 0 shear stress conditions, the data were interpreted to indicate that chronic culture of endothelial cells under shear stress markedly stimulated cell adhesion to the underlying material.
- 20
- 25      Scanning electron microscopy for cartridges with glomerular endothelial cells grown under 0 shear is shown in FIGURE 2, for cells grown at HFA in FIGURE 3. After adaptation to 0 shear conditions for 9 days, few cells remain sufficiently attached to withstand an  $\sim 10$  dyne/cm<sup>2</sup> flush (see also Table 1).

After adaptation to shear at 1.5 dyne/cm<sup>2</sup> followed by 15 dyne/cm<sup>2</sup>, cells do not detach from the fibers with a ~10 dyne/cm<sup>2</sup> flush. The large "craters" observed in some of the cells were only observed under arterial, not under venous levels of flow. As judged by transmission EM, these may represent areas of highly attenuated cytoplasm. It is not yet known whether this phenomenon also occurs in endothelial cells from large vessels.

RNA Isolation: Cells under varying shear stress/hydraulic pressure conditions were taken from the incubator and the cartridge was flushed with 30 cc of DEPC treated ice-cold PBS. The PBS was drained and immediately replaced with ice-cold 4.0 guanidine isothiocyanate (GTC) followed by shaking for 45 minutes (at 4°C). The GTC solution was then collected from the cartridge by pushing it back and forth in the fibers several times with syringes. The resulting material was then homogenized and total RNA recovered by ultracentrifugation on a cesium-TFA gradient. The usual yield for one confluent cartridge was ~300 µg total RNA. Poly (A)+RNA was then purified from total RNA using oligo(dT)-cellulose.

<sup>3</sup>[H]Thymidine incorporation: Cartridges were flushed with Hanks' balanced salt solution. The cartridges were then incubated for 3 hours with medium containing 2% serum and 1 µCi/ml <sup>3</sup>[H]Thymidine. The thymidine was removed, the fibers flushed/incubated 3 X 30 minutes with 6% ice-cold TCA, washed once with acetic methanol at -20°C, and dried. Individual fibers (equal lengths) were then cut from the cartridge, the cells in each fiber were solubilized and incorporation of radioactivity for individual fibers was determined.

EXAMPLE 3  
MORPHOLOGICAL STUDIES

Scanning and transmission EM studies were performed with cells grown for 9 days under various flow conditions. Morphological studies indicated a significant flattening of the cells grown under flow (FIGURE 4) and the expression of dense arrays of actin filaments and dense bodies at the base of the cells (FIGURE 5a) compared to a poorly developed array of actin filaments in cells grown on coverslips under static conditions (FIGURE 5b). In many areas cells grown under shear stress became extremely flattened with fenestrae formation (FIGURE 5c). To date, Weibel Palade bodies have not been seen on transmission EM of cells grown in static culture; they were easily found in cells grown under shear stress (FIGURE 5d). Finally, with regard to cell adhesion and confluence of the monolayers, FIGURE 5e shows a fiber end on, with the monolayer shrunken away from the polypropylene. The basolateral surface of the cells contains numerous projections, which are seen to "burrow" into the polypropylene fiber by transmission EM (FIGURE 5a). In FIGURE 5e, the fact that the monolayer is nearly complete is also well demonstrated.

FIGURE 4 shows that after adaptation to shear at 1.5 dyne/cm<sup>2</sup> for 7 days, glomerular endothelial cells take on an extremely flattened appearance. FIGURE 5a shows transmission EM of glomerular endothelial cells grown under flow (venous level shear stress, 9 days). Cells grown at any level of flow consistently showed a highly organized and dense array of actin filaments with dense bodies. The cells also contain a large number of ribosomes, suggesting a high rate of protein synthesis. Furthermore, the cells seemed to send anchoring projections into the underlying polypropylene fibers.

FIGURE 5b shows glomerular endothelial cells grown on a cover slip under static conditions (compare with FIGURE 5a). The cells contained few actin filaments and the density of ribosomes was less than that in cells grown under flow.

5 FIGURE 5c is an example of an extremely attenuated area of cytoplasm with 3 fenestrae. Whether the degree of fenestral development is a function of time and level of shear stress or merely represents a phenotypic change of endothelial cells grown on permeable supports is unknown. FIGURE 5d shows 10 an example of a Weibel Palade Body (large arrow). A mitochondrion in the same field (small arrow) is shown for comparison.

FIGURE 5e shows a polypropylene fiber containing glomerular endothelial cells adapted to shear for 9 days seen end on. The cells have lifted off the fiber during fixation. The basolateral cell surface (left lower corner) contains numerous anchoring projections. A circumferential monolayer is seen.

15

EXAMPLE 4  
MITOGEN SYNTHESIS

The effect of shear stress on the synthesis and secretion of mitogenic factors was studied. Given previous studies suggesting that glomerular hemodynamics may be causally related to glomerular sclerosis (Brenner, B., *Am. J. Physiol.* 249:F324, 1985), conditioned medium (no serum) from glomerular endothelial cells adapted to 0, venous or arterial levels of shear was examined for mitogenic activity on glomerular epithelial and mesangial cells. The cell to medium ratio was adjusted by dilution prior to determination of mitogenic activity.

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Control medium was not previously exposed to endothelial cells. There was a significant increase in mitogenic activity in medium harvested from glomerular endothelial cells under shear stress, though the level of shear stress did not significantly alter mitogen release. The findings for mesangial cell mitogenic activity were similar. FIGURE 6 shows the mitogenic effect of endothelial cell conditioned medium on quiescent glomerular epithelial cells.

FIGURE 7 shows total RNA was harvested from the endothelial cells under flow and subjected to Northern blot analysis with PDGF-A and PDGF-B chain cDNAs; hybridization with a cDNA for aldolase served to demonstrate equivalent loading. As can be seen, culture of glomerular endothelial cells under shear stress HFA and LFC markedly stimulated PDGF-B chain mRNA expression, though the level of shear stress did not have an independent effect. PDGF-A chain mRNA was much less abundant, and was not increased in cells exposed to shear stress. Therefore mitogenic activity in supernatants from glomerular endothelial cells grown under shear stress may be due to expression of PDGF.

**EXAMPLE 5**  
**STUDIES ON VASOACTIVE MEDIATORS**

Vasoactive mediator release by glomerular endothelial cells under shear stress was also studied. Cells were grown under static, LFC, HFA and HFC conditions in 10% serum for 9 days. Accumulation of 6-keto PGF<sub>1 $\alpha$</sub>  (prostacyclin metabolite) and endothelial-1 in the medium during the last 24 hours of culture was then determined by radioimmunoassay. Data points represent values for 3 separate experiments and were corrected for the medium volume : cell number ratio. FIGURE 8 shows 6-keto PGF<sub>1 $\alpha$</sub>  accumulation as a function of shear stress.

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All levels of shear stress significantly augmented 6-keto PGF<sub>1 $\alpha$</sub>  accumulation by comparison with static conditions. Furthermore, cells grown at arterial levels of flow either for 24 hours or 5 days released approximately 10 fold more 6-keto PGF<sub>1 $\alpha$</sub>  than cells grown at venous levels of shear. Thus, there was a  
5 chronic induction of prostacyclin release with arterial levels of shear stress, possibly reflecting continued activation of cell membrane signalling events, or possibly induction of the PLA<sub>2</sub> enzyme by high shear.

- Medium from the same cartridges as those used for experiments in FIGURE 8 was also assayed for endothelin-1 accumulation.  
10 Table 2 shows endothelin-1 accumulation (fmol/100  $\mu$ l) over 24 hours as a function of shear stress levels in three experiments.

TABLE 2

EXPT.	O SH.	LFC	HFA	HFC
1	544	1670	3970	1792
2	635	2372	1420	2740
3	552	12387	2820	7605

- 0 SH = No Shear Force.  
15 Endothelin-1 accumulation was much more variable than 6-keto PGF<sub>1 $\alpha$</sub>  accumulation (FIGURE 8). Medium from cells exposed to shear consistently contained more endothelin-1 than medium from static cells, though the level of shear stress had no apparent effect.  
20

EXAMPLE 6  
METHODS FOR PREPARATION OF  
ENDOTHELIAL CELL VASCULAR GRAFTS

Initiation of bovine endothelial cell culture

5      Bovine aortic endothelial cells (BAE) were harvested by collagenase digestion, plated at cloning density, and individual colonies were expanded as previously described (Ballermann, BJ, *Am J. Phys Cell*, 25:C182-9, 1989). Freshly isolated cells were cultured in RPMI 1640 (Gibco, Grand Island, NY) medium containing 10% FBS. Endothelial cell lines were determined to be homogeneous by  
10     fluorescent acetylated LDL uptake and/or factor VIII immunocytochemistry.

Cell seeding into vascular grafts

Flow chambers similar to those described by Shindo (S. Shindo, et al., *J. Vasc Surg.*, 6:325-32, 1987) were custom-produced by Small Parts Inc., (Miami Lakes, FL) and are shown schematically in FIGURE 9. A 1.5 mm corethane graft is shown fixed in the flow path. Medium can be circulated in separate circuit through the lumen of the graft, in the outer chamber around the graft, or both. The access ports of the chamber allow medium circulation through the inner lumen and/or in the outer chamber around the outer surface of the graft. Woven Corethane (Corvita Corp., Miami, FL) 1.5 mm internal diameter  
15     vascular grafts 4 cm in length were fixed into the flow path. The inner lumens of the grafts were first coated with 4% bovine gelatin (Sigma, St. Louis, MO) for 5 minutes, followed by ProNectin F (Protein Polymer Technologies, San Diego, CA) in sterile water (1:20) at room temperature for 2 hours. The inner and outer surfaces of the grafts were washed 3 times with sterile water, dried  
20     at 60°C for 4 hours, and then steam autoclaved. The graft lumen and outer chamber were filled with RPMI 1640 medium containing 1% FBS. The grafts were densely seeded with endothelial cells as follows. Two ml of suspended BAE ( $1-3 \times 10^7$  cells/graft) were injected into the graft lumen and incubated  
25

horizontally at 37°C in 5% CO<sub>2</sub>/95% air for 30 minutes. This step was repeated once, and the flow chamber and graft were rotated 180° around their long axis to ensure circumferential seeding. The inner lumen was then gently flushed with culture medium now containing 10% FBS. Culture medium was then 5 circulated in separate circuits, either to the inner lumen, outer chamber, or both, with gas permeable tubing connected to a CellMax Quad (Celco Inc., Germantown, MD) pump and reservoir system.

In each of three separate experiments, 4 grafts were studied. In each experiment two grafts were exposed to medium circulating through the outer 10 chamber only while medium in the lumen remained stationary. Since the endothelial cells within the graft lumens were not exposed to flow, these were the static controls. The two remaining grafts were exposed to shear stress by perfusing their lumens in addition to their outer chamber. To perfuse the graft lumens, the pump was initially set to deliver shear stress at 0.9 - 1.4 dynes/cm<sup>2</sup> 15 for 3 days followed by 3 days at 25.6 - 28.8 dynes/sm<sup>2</sup>. Shear stress in large veins has previously been estimated to be in the 1-4 dynes/cm<sup>2</sup> range, that for large arteries in the range of 10-30 dynes/cm<sup>2</sup>. Medium was circulated through the chamber surrounding all grafts at 5.5 - 6.5 mls/min. Nonseeded vascular 20 grafts were also prepared for two of the three experiments by coating them with bovine gelatin and ProNectin F and steam autoclaving them.

#### Acute shear stress protocol

At the completion of the 6 day culture period, the lumen of each vascular graft was exposed to shear stress at 25 dynes/cm<sup>2</sup> for 25 seconds with HBSS (Gibco, Grand Island NY) at 37°C. This was done to mimic the acute exposure 25 to shear stress, which would have occurred had the grafts been implanted in an artery. The medium was collected and the number of cells dislodged by acute shear stress was determined with an automated Coulter counter (Model

ZM, Coulter Electronics Limited, Luton, England). Each vascular graft was then divided into 3 equal parts.

The distal third was fixed in formalin for H&E staining, the middle third was used to determine clotting time, and the proximal third was fixed in 3% glutaraldehyde and processed for scanning electron microscopy as previously described (Ott M.J., et al., *J. Amer. Soc. Neph.*, **4**:564, 1993).

**Whole blood clotting time**

Surface thrombogenicity was determined with methods similar to those described by Yates (Yates S.G., et al., *Surg. Gyn. & Obst.*, **136**:12-6, 1973) with minor modifications. Briefly, the graft segments were closed at one end with a rubber shod vascular clamp. The grafts were then filled with 100  $\mu$ l of freshly drawn human volunteer blood and placed in a humidified chamber at 37°C. Adhesion of a reproducible fibrin thread to a wooden applicator stick was taken as the end point for the surface clotting time.

**Shear stress determinations**

A Newtonian fluid in a cylinder under laminar flow shear stress [ $t$ ] at the vessel wall is defined as:  $t = (4nQ)/(\pi r^3)$ , where  $n$  = viscosity,  $Q$  = fluid flow rate,  $r$  = internal radius (Goldsmith HL, et al., *Throm Haemost*, **55**:415-25, 1986). In these experiments each vascular graft had a uniform internal diameter of 1.5 mm. The flow rate was measured independently for each graft in each experiment and was laminar with a Reynold's number ( $Re$ ) =  $Qd/v < 25$ , where ( $d$ ) is the internal diameter of the graft in centimeters, and ( $v$ ) is the kinematic viscosity in Stokes. Viscosity of the culture medium was determined independently at 37°C with a Cannon-Manning semi-micro capillary tube viscometer size 50 (International Research Glassware, Kenilworth, NJ) and ranged from 0.74 to 0.76 centipoisesecs for RPMI 1640 containing 10% FBS. Shear stress was calculated independently for each vascular graft in each experiment and

was within the physiologic ranges representing venous ( $1\text{-}4$  dynes/cm $^2$ ) and arterial levels ( $10\text{-}30$  dynes/cm $^2$ ) in humans.

#### Statistical analysis

Duplicate grafts were examined in each experiment. All results are expressed  
5 as the mean of three separate experiments  $\pm$  standard error of the mean. Statistical analysis was performed using GB-STAT software (Dynamic Microsystems, Inc., Silver Spring, MD). For data in FIGURE 10 comparisons between groups were by the Student 2-tailed t-test. For data in FIGURE 12 comparisons between groups were by a Bonferroni adjusted t-test with pooled  
10 variance.

#### EXAMPLE 7

FIGURE 10 compares the number of cells dislodged by a 25 sec pulse of shear stress at 25 dynes/cm $^2$  from endothelial cell seeded grafts after 6 days of culture in the absence or presence of chronic sheer stress. On average,  
15  $1.32 \pm 0.44 \times 10^6$  cells were dislodged from the static grafts compared to  $1.05 \pm 0.16 \times 10^4$  cells from grafts preconditioned by shear stress ( $p<0.05$ ).

FIGURE 11 shows the appearance of the grafts by light and scanning electron microscopy. After exposure to an acute pulse of shear stress (25 dynes/cm $^2$  for 25 seconds). Panels A, C and E show grafts cultured with continuous  
20 shear stress for 6 days. Panels B, D and F show grafts cultured in the absence of luminal shear stress for 6 days. A, B: 60X; C, D: 160X (longitudinal sections, H & E stain). Intact monolayers of endothelial cells are shown on the luminal surface (L) of grafts cultured in the presence of shear stress ( $\rightarrow$ ). Few cells are present on the luminal surface of grafts cultured without luminal  
25 shear stress ( $\neg$ ). Cells are present on the abluminal surface ( $\uparrow$ ) and in the

interstices of the grafts. (E, F: Scanning electron microscopy of graft lumens, 100X). The luminal surface of grafts grown with shear stress is covered with cells, that of the grafts cultured in the absence of luminal shear stress contains few cells.

- 5       The inner lumen (L) of the shear stress conditioned grafts always contained an intact monolayer of endothelial cells, whereas few cells covered the inner lumen of grafts not preconditioned by shear stress. Endothelial cells were also found in the wall and on the abluminal surface of both shear stress conditioned and unconditioned grafts.
- 10      FIGURE 12 shows *in vitro* clotting times in vascular grafts without endothelial cells ( $n = 4$ ), in grafts seeded with endothelial cells and then grown under static conditions ( $n = 6$ ), and in grafts conditioned by shear stress ( $n = 6$ ). Lines connect individual data points obtained from grafts within a single experiment and with the same blood sample. The clotting time was  $41 \pm 4$  percent longer in grafts cultured with luminal shear stress compared to grafts cultured without luminal shear stress ( $p < 0.01$ ). In all experiments, the presence of endothelial cells in the vascular graft significantly prolonged the clotting time compared to grafts without cells. In addition, the whole blood clotting was more prolonged in grafts containing endothelial cells that had been preconditioned by shear stress compared to grafts cultured without flow. On average, the clotting time was  $41 \pm 4$  percent longer in shear stress conditioned grafts compared to grafts from static cultures ( $p < 0.01$ ).

- 20      In the present invention, endothelial cells were seeded on vascular graft material followed by 6 days of culture in the presence or absence of continuous shear stress. A brief exposure of the endothelial cell seeded grafts to arterial levels of shear stress was then used to simulate the initial hemodynamic force endothelial cells would experience were the grafts implanted. Exposure

- to a 25 sec interval of arterial level shear stress dislodged approximately 100 fold more cells from the static grafts compared to those that had been cultured for 3 days under venous and then an additional 3 days under arterial shear stress. Taken together with the observations from light and scanning electron microscopy, that the inner lumen of shear stress conditioned grafts was covered by intact endothelial cell monolayers whereas the inner surface of static grafts contained few cells, these findings are interpreted to indicate that shear stress stimulates endothelial cell adhesion to the graft material such that the monolayers can resist disruption by shear stress.
- 5
- 10 The foregoing is meant to illustrate, but not to limit, the scope of the invention. Indeed, those of ordinary skill in the art can readily envision and produce further embodiments, based on the teachings herein, without undue experimentation.

**CLAIMS**

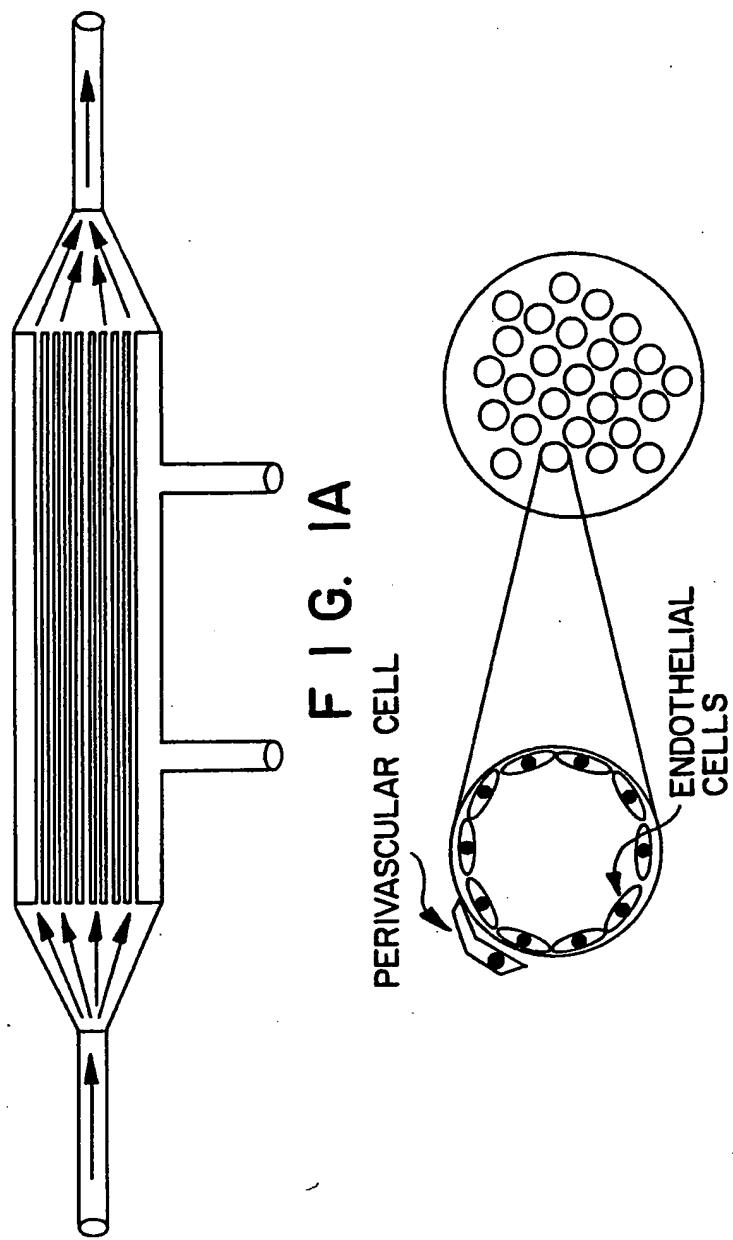
1. A method for producing a device having a surface coated with an adherent cell monolayer which comprises culturing the adherent cells with the device under continuous shear stress from 0.4 dyne/cm<sup>2</sup> to 33 dyne/cm<sup>2</sup> to produce the monolayer.
2. The method of claim 1, wherein the cells are endothelial cells.
3. The method of claim 1, wherein the device is an implantable biomaterial for implanting in a subject.
4. The method of claim 3, wherein the implantable biomaterial is a prosthetic vascular device.
5. The method of claim 1, wherein the device contains at least one hollow fiber.
6. The method of claim 1, wherein the cells forming the adherent cell monolayer are co-cultured with a second population of cells in the device wherein the second population of cells are phenotypically distinct from the cells of the adherent cell monolayer.
7. The method of claim 5, wherein the cells are grown in the inner lumen of the hollow fiber.
8. The method of claim 5, wherein perivascular cells are grown on the outer lumen of the hollow fiber.

9. The method of claim 8, wherein the perivascular cells are selected from the group consisting of vascular smooth muscle cells, mesangial cells, pericytes, fibroblasts and epithelial cells.
10. The method of claim 1, wherein the device is made of polypropylene material.
11. The method of claim 1, wherein the cells are stably transfected with at least one gene.
12. The method of claim 11, wherein the gene encodes a protein which reduces thrombogenicity.
13. The method of claim 12, wherein the gene is selected from the group consisting of t-PA and PLA<sub>2</sub>.
14. The method of claim 11, wherein the gene encodes a vasodialating mediator.
15. The method of claim 11, wherein the gene encodes an angiogenic factor.
16. The method of claim 1, wherein the device is pre-coated with an extracellular matrix protein.
17. The method of claim 16, wherein the extracellular matrix protein is selected from the group consisting of fibronectin, laminin, and collagen.
18. The method of claim 1, wherein the shear stress is from 1 dyne/cm<sup>2</sup> to 14 dyne/cm<sup>2</sup>.

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19. A device coated with an adherent cell monolayer according to the method of claim 1.

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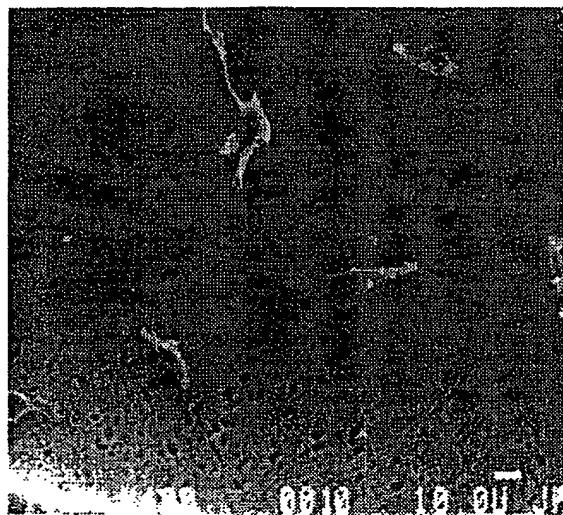


FIG. 2

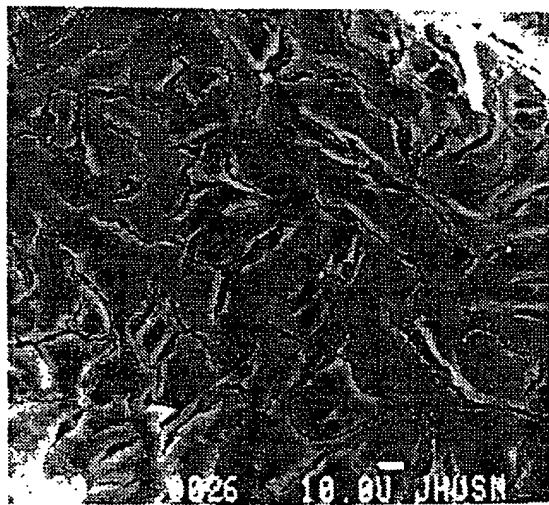


FIG. 3

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**FIG. 4**



**FIG. 5a**

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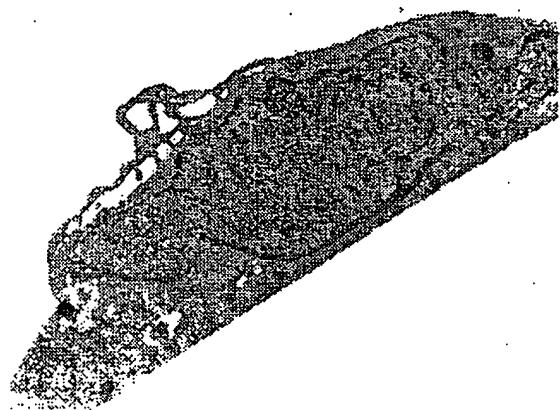


FIG. 5b



FIG. 5c

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FIG. 5d

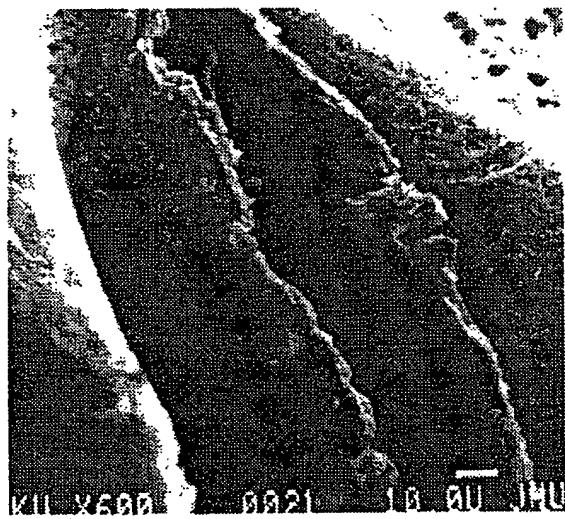


FIG. 5e

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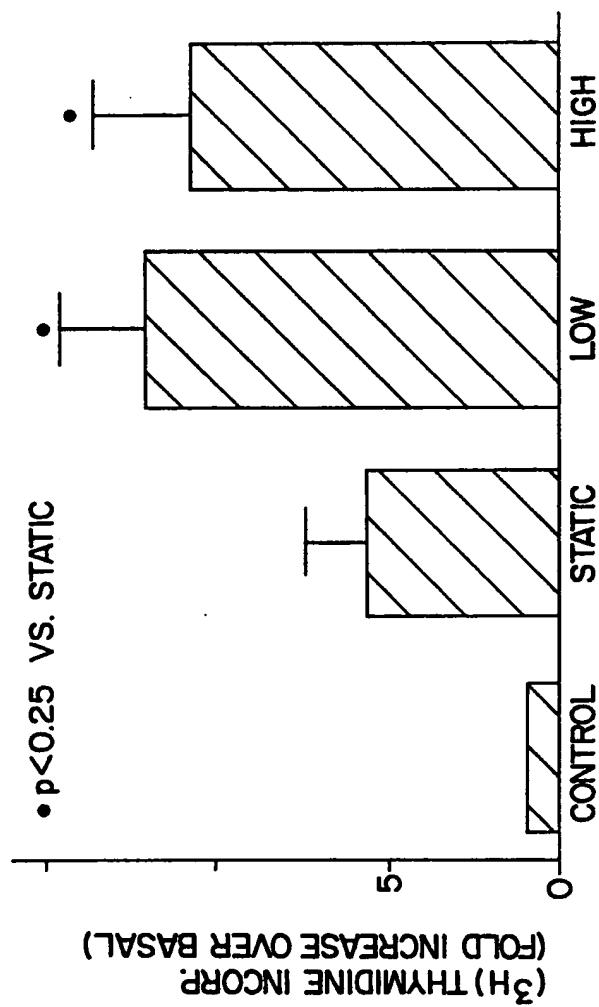
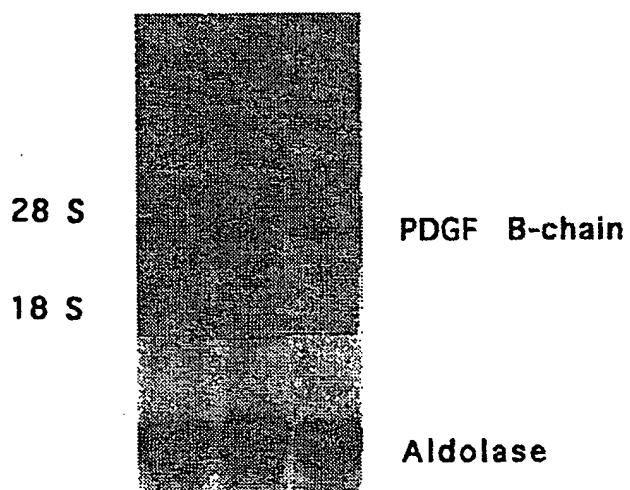


FIG. 6

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**HFA LFC 0 Shear****F I G. 7****SUBSTITUTE SHEET (RULE 26)**

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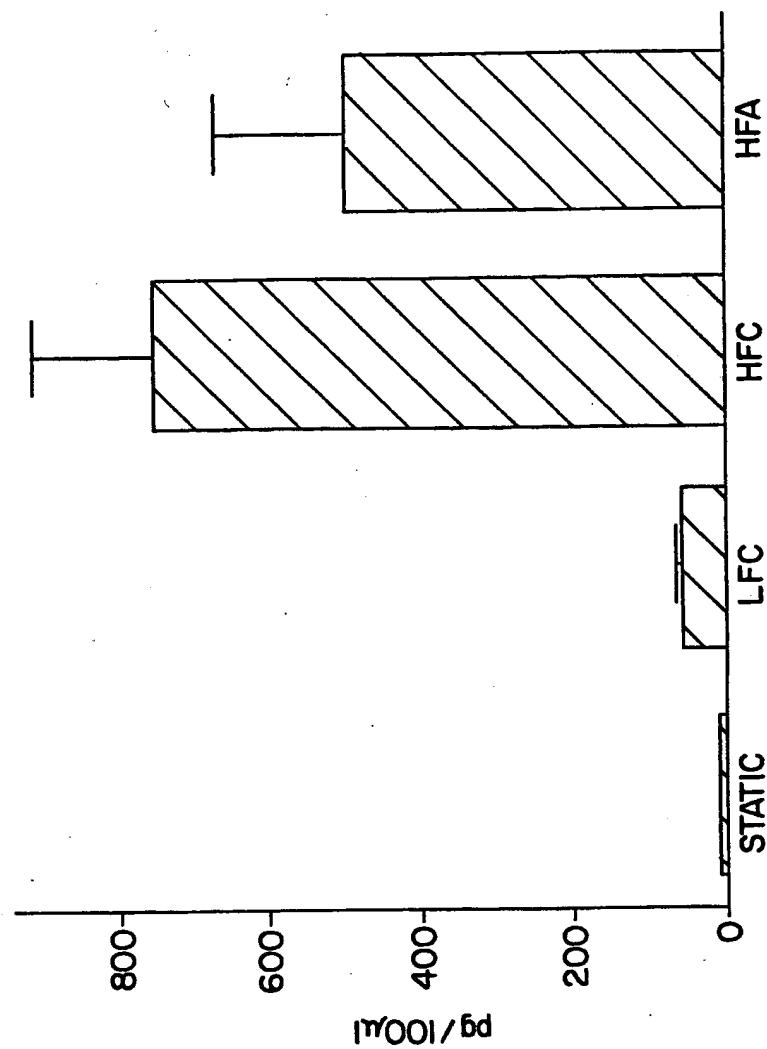


FIG. 8

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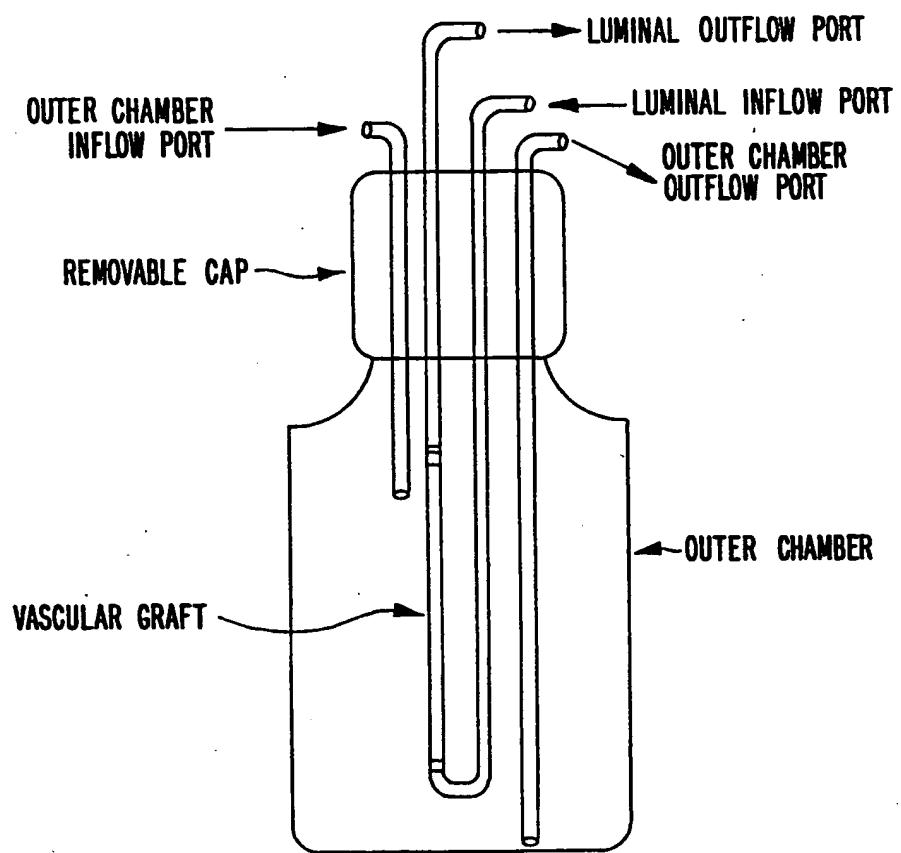


FIG. 9

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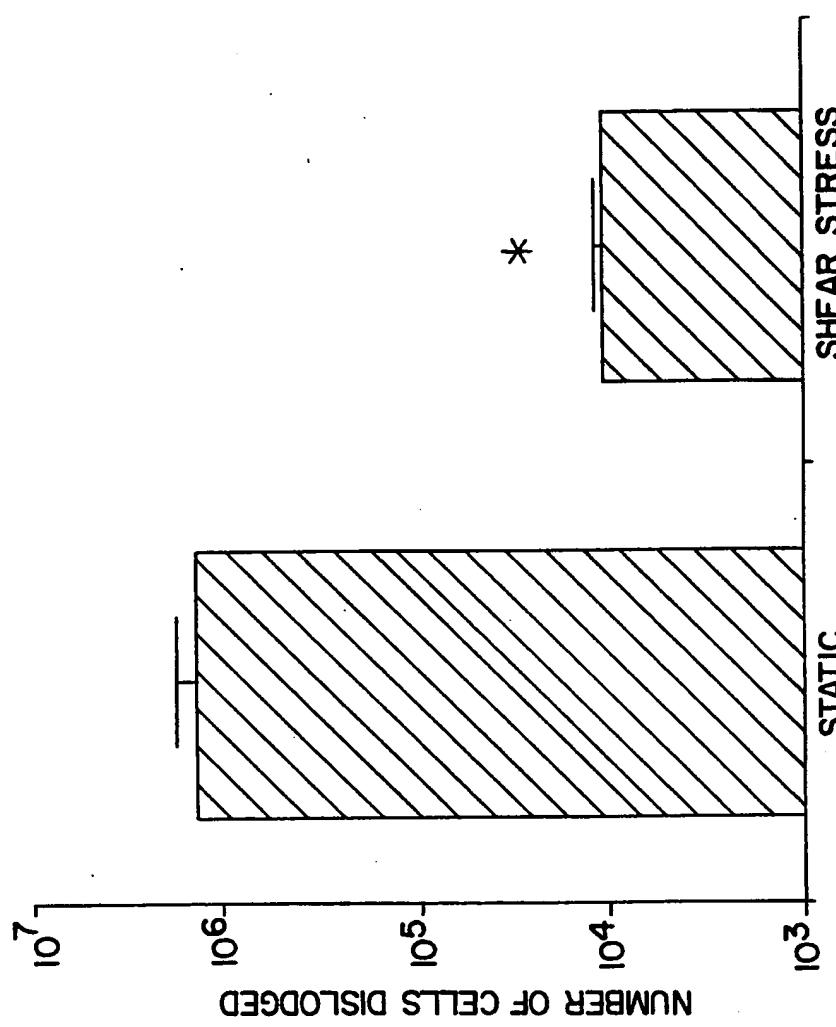


FIG. 10

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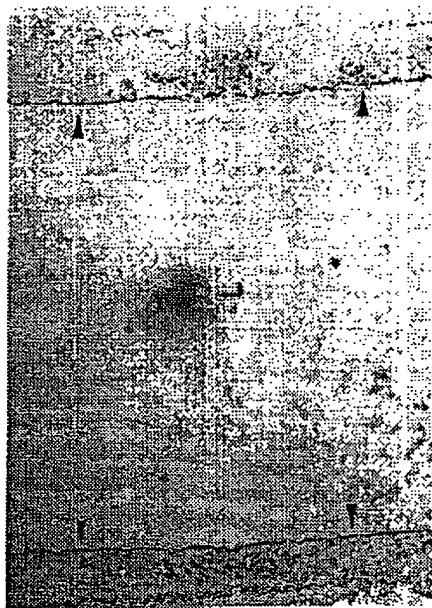


FIG. II B

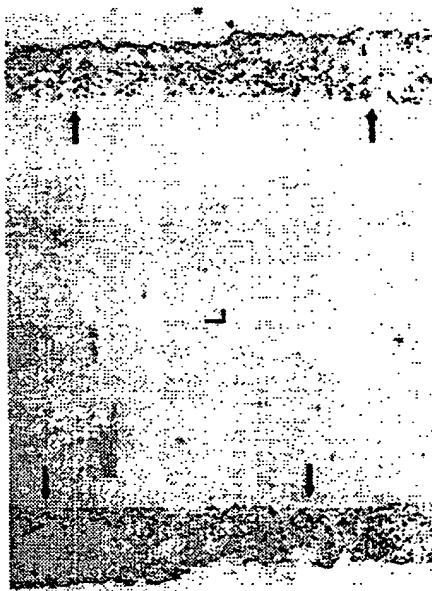


FIG. II A

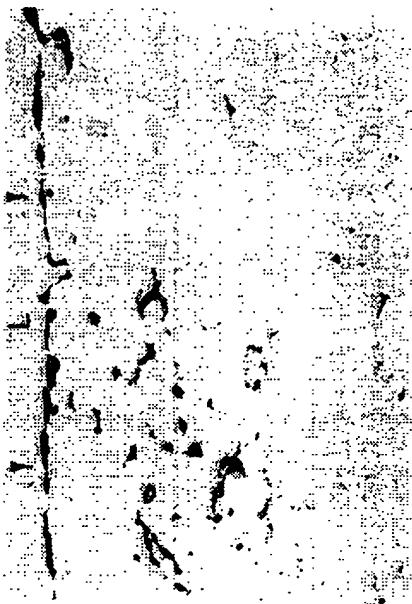


FIG. II D



FIG. II C

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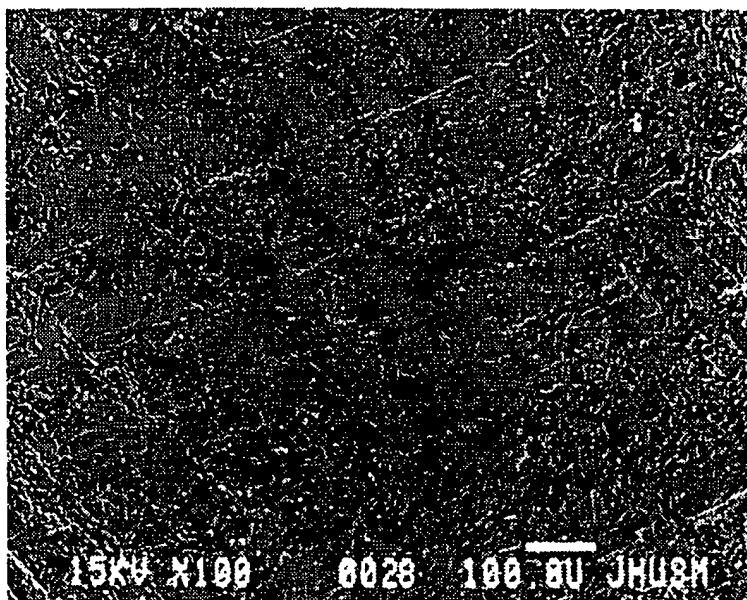


FIG. II E

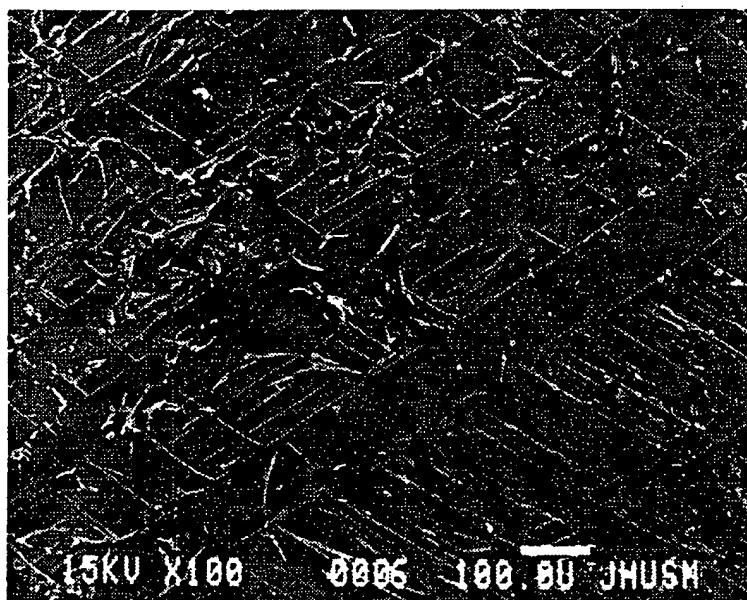


FIG. II F

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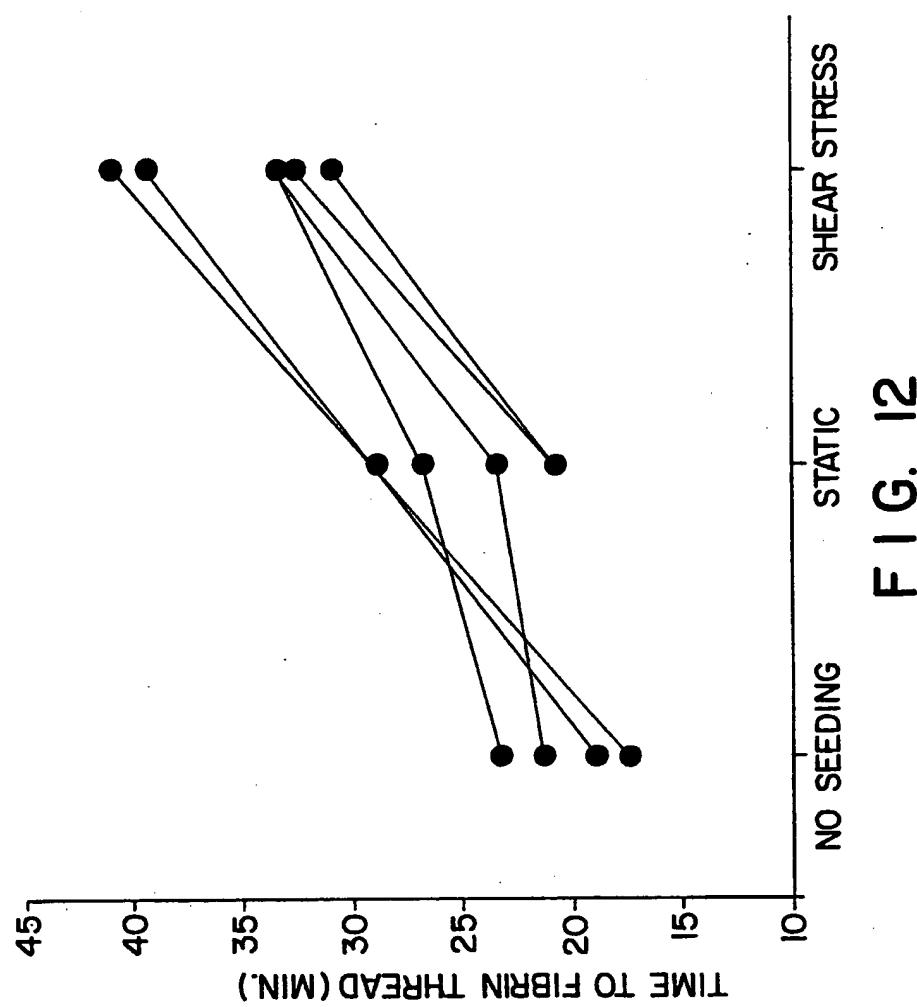


FIG. 12

## INTERNATIONAL SEARCH REPORT

International application No.

PCT/US94/04663

**A. CLASSIFICATION OF SUBJECT MATTER**

IPC(5) :C12N 11/08, 5/00

US CL : 435/180, 240.23, 240.243

According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 435/180, 240.23, 240.243

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

APS, CAS, MEDLINE, BIOSIS

search terms: cell, monolayer, shear stress, hollow fiber, lumen, implantable, vascular

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	International Journal of Microcirculation: Clinical and Experimental, Volume 9, issued 1990, Höhn et al, "Seeding of Endothelial Cells in Perfused Microporous Glass Capillaries", pages 411-422, entire document.	1, 2, 16, 18, 19 -----
Y	US, A, 3,883,393 (KNAZEK ET AL) 13 May 1975, entire document.	3, 4-15, 17
Y	US, A, 4,804,628 (CRACAUER ET AL) 14 February 1989, entire document.	5, 7, 8, 9
Y	US, A, 5,037,378 (MULLER ET AL) 06 August 1991, entire document.	5, 7, 8, 9
Y	US, A, 5,162,225 (SAGER ET AL) 10 November 1992, entire document.	1-19
Y		1-19

Further documents are listed in the continuation of Box C.

See patent family annex.

- \* Special categories of cited documents:
- "A" document defining the general state of the art which is not considered to be of particular relevance
- "E" earlier document published on or after the international filing date
- "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
- "O" document referring to an oral disclosure, use, exhibition or other means
- "P" document published prior to the international filing date but later than the priority date claimed

- "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
- "X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
- "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
- "&" document member of the same patent family

Date of the actual completion of the international search

03 AUGUST 1994

Date of mailing of the international search report

10 AUG 1994

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